

Foamy oil and wormhole footprints...

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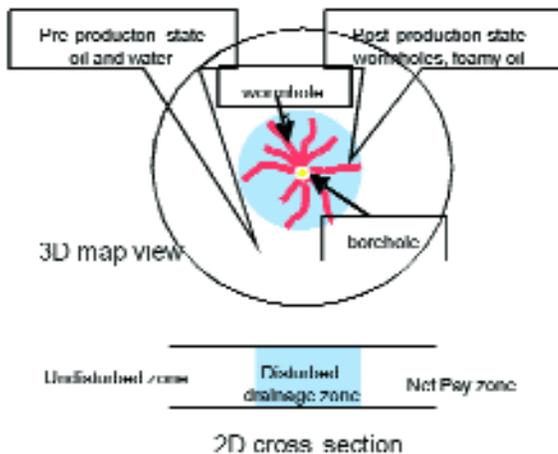


Figure 3 Simplified drainage model with foamy.

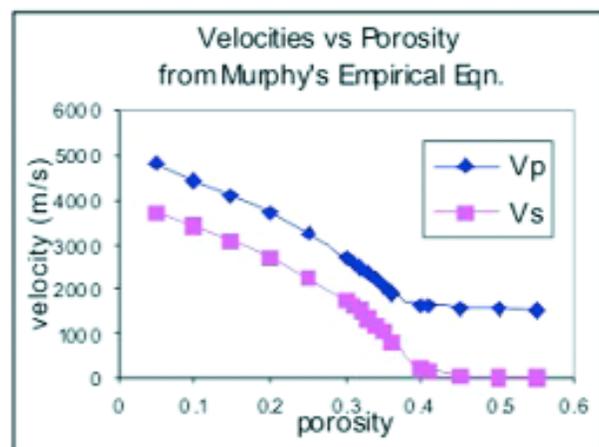


Figure 5. Velocity vs porosity of porous sands

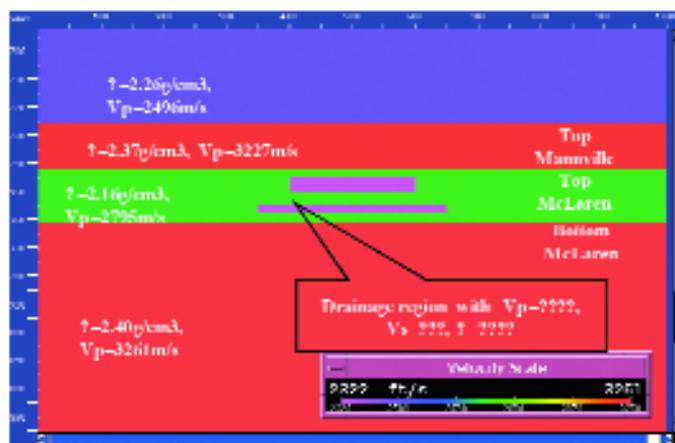


Figure 4 2D post-production geological model oil and wormholes with drainage zones.

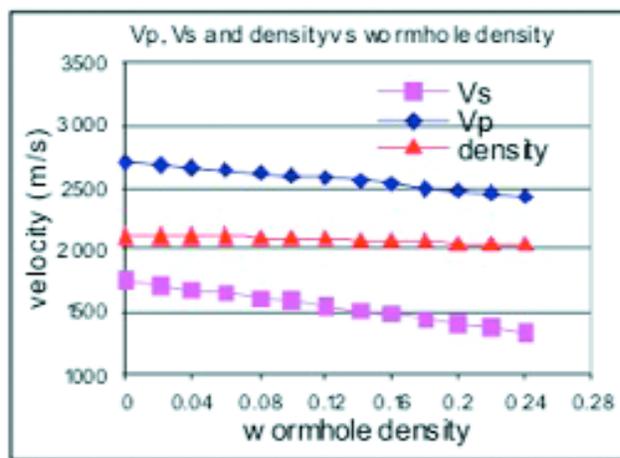


Figure 6. Velocity and density of drainage sands from Murphy's empirical relations vs. wormhole density, where wormhole porosity defined as 50%, reservoir sand porosity as 30%.

Physical Properties of Drainage Zones With Foamy Oil Effects	Pre-production $S_g=0, S_o=0.8$	Post-production $S_g=0.1, S_o=0.7$		
		Reuss	Voigt	Average
Saturated Rock Bulk Modulus (Gpa)	10.616	5.2252	10.113	7.807
Saturated Shear Modulus (Gpa)	4.6726	4.6777	4.6777	4.676
Saturated Bulk Density (kg/m^3)	2156.5	2126.6	2126.6	2126
V_p (m/s)	2795	2325	2773	2570
V_s (m/s)	1472	1483	1483	1483

Table 1. Rock properties of drainage sands with the presence of foamy oil. As reservoir pressure decreases from 3MPa to 1.5MPa, S_o changes from 80% to 70%, and S_g from 0 to 10%.

cylinder around boreholes. A schematic of this is shown in Figure 3. The volume of the drainage zone is determined by the length of wormholes and the net pay thickness. 2D numerical models are built based on well logs of the pre-production model in a Canadian cold production field. Figure 4 only shows the post-production model with two drainage zones. They are respectively 5m and 3m thick, and 200m and 300m long.

It is necessary that some manner of defining the P -wave, S -wave velocities V_p and V_s and density ρ of the drainage zones be adopted. Foamy oil effects have been computed by applying Reuss lower and Voigt upper bounds, where the moduli for gas,

water and heavy oil were calculated from the equations in Batzle and Wang (1992). The results are given in Table 1. With 10% of gas in solution V_p decreases significantly using the lower bound but changes only minimally when the upper bound is used. Slight increases of densities are due to exsolved gas taking the place of heavy oil. As a consequence of the uncertainty in estimating the elastic parameters of fluid mixture, the averages of V_p , V_s , and ρ from Reuss and Voigt bounds have been used in the modeling procedure.

Wormholes with porosities greater than the critical porosity, have sand grains suspended within the fluid. Therefore, the empirical relations between moduli and porosity of pure sands (Murphy et al, 1993) have been used to calculate elastic moduli of wormhole sands, and Gassmann's equations applied to obtain both P - and S -wave velocities. Figure 5 shows that both V_p and V_s decrease with increasing porosity. V_s tends to be zero when the porosity is greater than the critical porosity, because the sand grains become fluid-supported.

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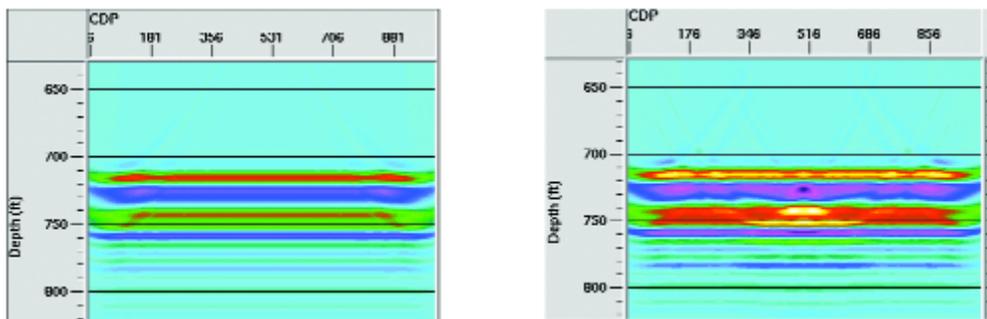


Figure 7. Migrated sections of pre- (left) and post-production (right) models with foamy oil effects.

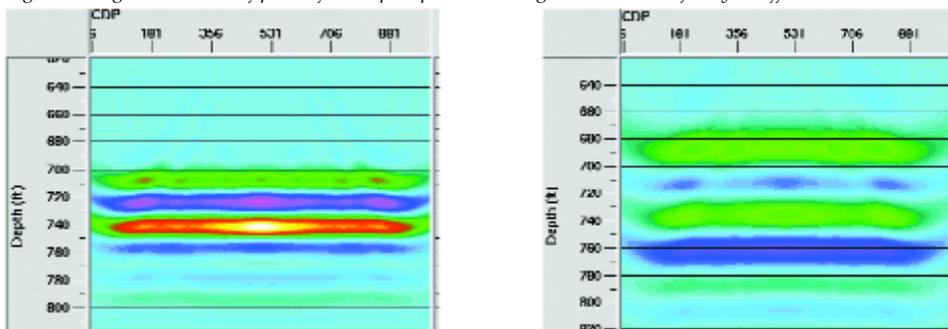


Figure 8 Migrated sections of post-production model using 100Hz (left) and 50Hz (right).

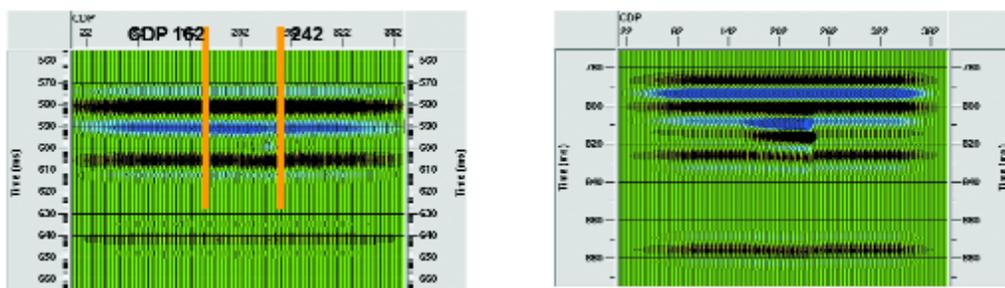


Figure 9. Stacked sections of PP(left) and PS(right) of post-production models with wormholes

The macroscopic effects of wormholes, ignoring any foamy oil influence, on V_p and V_s within the drainage sands can be observed. These velocities have been obtained by using Voigt upper bound. The reductions of V_p and V_s are proportional to the wormhole density. The decrease in V_s appears more rapid, while ρ changes little (Figure 6).

Modeling results and conclusions

Seismic responses of foamy oil models

The pre-production model and the two-drainage zone model (shown in Figure 4) have been used to generate zero-offset seismograms, with V_p and ρ taken from Table 1 and using a zero-phase wavelet with frequency bandwidths of 200Hz, 100Hz and 50Hz respectively. Figure 7 shows the depth migrated sections of the pre- and post-production model for a 200Hz frequency bandwidth. The amplitude anomalies and traveltimes delays caused by the low velocity drainage zones filled with gas bubbles are evident. At a frequency bandwidth of 100Hz, the cumulative responses of the two drainage zones become one anomaly (Figure 8), rather than the two in Figure 7. With a 50Hz frequency bandwidth any anomalies are difficult to observe (Figure 8).

Seismic Response of Wormhole Models

The post-production model, shown in Figure 4, has been slightly modified including only the upper drainage zone, which has been divided into 10 lateral blocks. A wormhole density increase from 2% to 20% in adjacent blocks is incorporated, corresponding to V_p varying from 2688m/s to 2478m/s and V_s from 1717m/s to 1404m/s. Ray tracing modeling has been employed using a 60Hz Ricker wavelet.

The stacked PP and PS seismic sections are shown in Figure 9. The drainage zone disturbed by wormholes lies between CDP 162 and 242. Because of the greater contrasts in V_s , the amplitude anomalies and travel time delays on the PS section are more readily seen than on the PP section, where only subtle changes can be detected around CDP 240 where high wormhole densities exist. The increases in amplitudes from CDP 162-242 are proportional to the increase of wormhole density, thus possibly predicting the relations between wormhole footprints and amplitude variations. A reason for PS data having higher resolution could be due to its relatively short wavelength compared with that of PP data for similar frequencies.

We may conclude that both PP and PS data could be tools to aid in delineating the footprints of foamy oil and wormholes. PP data is a useful tool imaging foamy oil effects because the fluid changes are sensitive to the P-wave velocity. While the presence of wormholes strongly affects the S-wave velocity, the reflected PS data can also be used to detect the most likely wormhole growing pattern, thus providing possible drainage indicators for infill drilling designs and development plans. As most of cold production reservoirs are thin, high frequencies are required to achieve discernible resolution.

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